# Determination of Energy Minima and Saddle Points Using Multireference Configuration Interaction Methods in Combination with Reduced Gradient Following: The S<sub>0</sub> Surface of H<sub>2</sub>CO and the T<sub>1</sub> and T<sub>2</sub> Surfaces of Acetylene

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Received 12 September 2001; Accepted 25 November 2001:

**Abstract:** The implementation of the reduced gradient following (RGF) method into the COLUMBUS quantumchemical program system is reported using the newly developed analytic MR-CISD/AQCC gradient feature. By this combination a very useful tool has been developed for general searches of stationary points on ground- and excited-state energy surfaces. This procedure is applied to the S<sub>0</sub> surface of H<sub>2</sub>CO and the T<sub>1</sub> and T<sub>2</sub> surfaces of acetylene. For H<sub>2</sub>CO we investigated three minima (formaldehyde, *s*-trans, and *s*-cis hydroxycarbene) and five saddle points. For the T<sub>1</sub> and T<sub>2</sub> states of acetylene the *cis*- and *trans*-minima and the planar and nonplanar saddle points were computed.

© 2002 Wiley Periodicals, Inc. J Comput Chem 23: 576-583, 2002; DOI 10.1002/jcc.10054

Key words: saddle point search; reduced gradient following; analytic gradients for excited states; H<sub>2</sub>CO; acetylene

## Introduction

Stationary points play a fundamental role for the characterization of potential energy surfaces (PES). In most cases the determination of local minima can be regarded as routine work, because several reliable algorithms are available for that purpose (for reviews see, e.g., refs. 1 and 2). However, the search for saddle points on the PES is significantly more complex and is a nontrivial task even for smaller molecules.<sup>1,2</sup> The situation is more complicated by the fact that saddle point structures frequently contain significantly stretched chemical bonds and it is, therefore, not always clear whether single reference (SR) methods are sufficient for an accurate description of such structures. The investigation of excitedstate surfaces poses still more severe requirements on the quantum chemical method to be used and systematic searches even for minima are much less frequent than corresponding investigations for electronic ground states. In such critical cases multireference (MR) methods are required from which the multireference configuration interaction with singles and doubles (MR-CISD),<sup>3</sup> complete active space (CAS),<sup>4</sup> perturbation theory to second order (CASPT2),<sup>5</sup> and multireference averaged coupled pair functional (MR-ACPF)<sup>6</sup> or multireference averaged quadratic coupled cluster (MR-AQCC)<sup>7,8</sup> are mentioned here. The latter two methods are of interest because they allow the computation of size-extensivity corrections for MR cases based on a variational approach in close analogy to the CI method.

The availability of analytic gradients is, of course, an important practical criterion for the choice of an appropriate computational method for geometry searches. In contrast to the situation found for the SR case, analytic gradients are not so commonly available for MR methods. Many geometry optimizations are being performed only at the multiconfiguration self-consistent field (MCSCF) level. The omission of major parts of dynamic correlation in this approach may lead to significant artifacts. In the last years an efficient MR-CISD gradient method has been developed<sup>9-11</sup> and implemented into the COLUMBUS program system.<sup>12-15</sup> Because of the variational character of the above-mentioned MR-ACPF/AQCC methods, analytic gradients can also be computed for these methods in close analogy to the MR-CISD formalism. So far, this gradient formalism has been restricted to MR-CISD calculations based on single-state MCSCF, making the balanced treatment of excited states difficult. Recently, an extension of the MR-CISD gradient method based on state-averaged MCSCF calculations has been developed,16 concentrating in par-

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Contract/grant sponsor: Austrian Science Fund; contract/grant number: Special Research Program F16 and project P14442-CHE

Contract/grant sponsor: COST Chemisty/D9; contract/grant number: project No. D9/0006/98

Contract/grant sponsor: Deutsche Forschungsgemeinschaft (M. H.)

ticular on the treatment of excited states. In this implementation local minima and saddle points were determined by the direct inversion in the iterative subspace method for geometry optimization (GDIIS),<sup>17</sup> requiring starting geometries close to the stationary point. Global saddle point searches could not be performed so far within COLUMBUS.

It is the aim of this work to report the implementation of the reduced gradient following (RGF) method, recently developed by Quapp et al.,<sup>18-20</sup> into COLUMBUS as a tool for global searches of ground- as well as of excited-state PES. The RGF method has been shown to be very flexible and efficient in locating a large variety of saddle points. The computational aspects of saddle point searches using MR quantum chemical methods are similar to those for the SR case. However, there are a number of important practical questions of special interest for MR implementations due to the usually much longer computer times required for a given molecule as compared to SR calculations. Most importantly, second derivatives have to be computed as finite differences of analytical gradients in the present implementation because analytic second derivatives in the MR-CISD approach are not available due to the complexity of the formalism. Because in global PES searches knowledge of the exact Hessian is not necessary, we investigated various possibilities for its approximate evaluation (e.g., simple estimates, update schemes, and quantum chemical calculation with lower-level methods) with the aim of finding a good balance between computational efficiency for the calculation of the Hessian and its reliability, which is still needed for satisfactory convergence of the RGF iterations.

In this work two applications are reported. The first one refers to the determination of minima and saddle points on the So surface of the H<sub>2</sub>CO system. Early studies have been performed at MCSCF,<sup>21</sup> SCF and CISD,<sup>22,23</sup> and Moller-Plesset perturbation theory<sup>24,25</sup> levels. These investigations already covered the most important stationary points. More recently, saddle points on S<sub>0</sub> have been studied at the coupled cluster,<sup>26</sup> density functional theory (DFT),<sup>27,28</sup> and quadratic configuration interaction with single, double, and triple [QCISD(T)] levels.<sup>29</sup> The most complete investigation on the barrier to unimolecular dissociation to  $H_2$ +CO has been undertaken by Feller et al.<sup>30</sup> Extended systematic studies of the S<sub>o</sub> surface using relatively small basis sets have been performed by Quapp et al.,<sup>18</sup> Jensen,<sup>31</sup> and Bondensgård and Jensen,<sup>32</sup> where additional interesting minima and first- and higher-order saddle points have been found and characterized. To our knowledge, no systematic investigations on saddle point structures using MR methods have been undertaken so far. The formaldehyde example is used to investigate the stability of the RGF implementation and to perform new high-level geometry optimizations using the MR-CISD and MR-AQCC methods.

In the second example, stationary points (*cis*- and *trans*-minima, in-plane and out-of-plane saddle points) on the PES of the first two excited triplet states ( $T_1$  and  $T_2$ ) of acetylene are investigated. These states have been studied previously by various authors.<sup>33–39</sup> In these investigations only planar structures have been optimized. In the work by Cui et al.,<sup>40,41</sup> systematic studies on the energy surfaces of several excited states of acetylene, including nonplanar structures, have been performed using the CASSCF and equation-of-motion coupled cluster with single and double (EOM-CCSD)<sup>42</sup> methods. In the case of the CASSCF optimizations, substantial fractions of dynamic electron correlation are missing, and in the case of EOM-CCSD the calculations are restricted to SR character. The present investigations comprise the first complete geometry optimizations for the T<sub>1</sub> and T<sub>2</sub> states of acetylene using multireference methods and are part of a general, systematic survey of planar and nonplanar sections of the T<sub>1</sub>–T<sub>4</sub> and S<sub>1</sub>–S<sub>2</sub> PES of acetylene.<sup>43</sup>

# **Review of the RGF Procedure**

In the RGF method,<sup>18</sup> which is a generalization of the distinguished coordinate method,<sup>44</sup> the gradient criterion for stationary points

$$\nabla E(\mathbf{x}) = \mathbf{0} \tag{1}$$

is reduced by one equation leading to

$$\frac{\partial E(\mathbf{x})}{\partial x^{i}} = 0, \quad i = 1, \dots, k, \dots, N$$
(2)

where the vector **x** represents the nuclear coordinates. In the original formalism<sup>18</sup> the search direction was defined by one individual coordinate,  $x^k$ . This formalism was generalized to an arbitrary, fixed search direction, **r**, by using the projector equation:<sup>19</sup>

$$\mathbf{P}_{\mathbf{r}}\nabla E(\mathbf{x}) = \mathbf{0} \tag{3}$$

where  $\mathbf{P_r}\mathbf{r} = \mathbf{0}$  for the fixed search direction  $\mathbf{r}$ . Note that eq. (2) is a special case of eq. (3) with the corresponding  $(N - 1) \times N$  projector matrix:

$$\mathbf{P_r} = \begin{pmatrix} 1 & \cdots & 0 & 0 & 0 & \cdots & 0 \\ \cdot & \cdots & \cdot & \cdot & \cdot & \cdots & \cdot \\ 0 & \cdots & 1 & 0 & 0 & \cdots & 0 \\ 0 & \cdots & 0 & 0 & 1 & \cdots & 0 \\ \cdot & \cdots & \cdot & \cdot & \cdot & \cdots & \cdot \\ 0 & \cdots & 0 & 0 & 0 & \cdots & 1 \\ \text{column} & 1 & k-1 & k & k+1 & N \end{pmatrix} \xrightarrow{\text{row}} (4)$$

Thus,  $\mathbf{P}_{\mathbf{r}}$  is built from the unit vectors orthogonal to the search direction where again the *k*th unit vector is missing. These reduced gradients of eqs. (2) and (3) define curves connecting stationary points. Starting from a given point (e.g., a minimum) one follows a selected curve to reach the saddle point of interest. A predictor-corrector method is used for tracing these curves. Assuming a curve of points  $\mathbf{x}(t)$  fulfilling the N - 1 conditions of eq. (3), the tangent  $\mathbf{x}'$  to the curve defined by eq. (3) is given as

$$\frac{d}{dt} \mathbf{P}_{\mathbf{r}} \nabla E(\mathbf{x}(t)) = \mathbf{0} = \mathbf{P}_{\mathbf{r}} \frac{d}{dt} \nabla E(\mathbf{x}(t)) = \mathbf{P}_{\mathbf{r}} \mathbf{H}(\mathbf{x}(t)) \frac{d\mathbf{x}(t)}{dt}$$
(5)

or

$$\mathbf{P}_{\mathbf{r}}\mathbf{H}(\mathbf{x}(t))\mathbf{x}' = \mathbf{0} \tag{6}$$

This is a homogeneous system of N - 1 linear equations where the coefficients are the elements of the Hessian matrix **H** projected by  $\mathbf{P_r}$ . Eq. (5) is solved using a *QR* decomposition. In the predictor step the sequence of points  $\mathbf{x}_m$  and  $\mathbf{x}_{m+1}$  is computed as

$$\mathbf{x}_{m+1} = \mathbf{x}_m + \frac{StL}{\|\mathbf{x}_m'\|} \mathbf{x}_m' \tag{7}$$

where StL is a steplength parameter.

Because the new point does not satisfy exactly the condition defined in eq. (3), a corrector step is added in which eq. (3) is solved using a Newton–Raphson-like method. In general, the linear combination  $\mathbf{r}$  of internal coordinates is used as an initial search direction. For further details of the procedure see refs. 18 and 19 and the web page.<sup>20</sup> The use of the metric in internal coordinates is explained in the appendix of ref. 45.

With the RGF method only the global search for a stationary point is performed. For final refinement the GDIIS method<sup>17</sup> is used.

#### **Computational Details**

All calculations were performed using the COLUMBUS quantumchemical program system.<sup>12–15</sup> Analytical gradients<sup>9–11,16</sup> of the energy with respect to nuclear coordinates were computed for the MR-CISD<sup>3</sup> and MR-AQCC<sup>7,8</sup> methods. Second derivatives were computed from finite differences of analytic gradients. The atomic orbital (AO) integrals and the AO derivative integrals were calculated using program modules taken from DALTON.<sup>46</sup> The extended Davidson method (MR-CISD+Q)<sup>47,48</sup> was used in single point calculations. The RGF and GDIIS<sup>17</sup> optimizations were performed in natural internal coordinates as defined by Fogarasi et al.<sup>49</sup> The harmonic vibrational frequencies were computed by the program SUSCAL developed by Pongor.<sup>50</sup>

## **Results and Discussion**

#### Hessian Update in the RGF Procedure

It should be noted that the criterion for the RGF curve [eq. (3)] does not use the Hessian. Therefore, it will be sufficient to use approximations to the Hessian via update methods.<sup>2</sup> Necessary evaluations of the Hessian needed are generally crucial and time consuming steps, especially in the present MR-CISD case where the Hessian is computed by finite differences from analytic gradients. Quite generally, one will try to perform global saddle-point searches at the lowest computational level possible because of the large computational costs involved in such searches. MCSCF calculations will usually constitute a good starting point. However, in some cases MR-CISD calculations will be required from the beginning because of artificial MCSCF results. The complexity of choices of appropriate procedures is certainly much larger for excited-state calculations as compared to the ground state. No general rules can be given in this case. The present COLUMBUS implementation offers for that purpose a variety of possibilities

with respect to methods used for RGF gradient calculations and for Hessian evaluation, which can be adapted to the respective situation. Some of these possibilities are demonstrated in the following examples.

Several options for approximating the Hessian were investigated. The first one (case 1) is to recompute the Hessian matrix at every point of the RGF search. This is the most expensive case and is intended to serve only as reference for further approximations. A second possibility (case 2) is to calculate the Hessian matrix once at the beginning of the RGF search and use a Hessian update method for all remaining iterations. For this update the method developed by Bofill<sup>51</sup> is used. Case 2 is the cheapest procedure, which will, however, depend significantly on the quality of the Hessian update algorithm. In order to have an alternative to this update-only procedure, we compute in case 3 the Hessian for each predictor step (because the largest geometry changes occur in this step) and use the Hessian update only for the corrector steps. As already noted above, it will not be necessary to compute the Hessian with the same high-level method that is used for the gradient. Either reduced basis sets or a low-level quantum chemical method (such as SCF or MCSCF) will suffice.

Two test examples for the RGF search were chosen: the sequence  $M_3 \rightarrow F_1 \rightarrow M_4$  for the out-of-plane saddle point  $F_1$ located between the *s*-trans (M<sub>3</sub>) and *s*-cis (M<sub>4</sub>) hydroxycarbene (see Fig. 1), and the out-of-plane saddle point located between the *cis*- and *trans*- minima on the PES for the T<sub>1</sub> state of acetylene. For the hydroxycarbene calculations the REDVAL MCSCF wave function and the REDVAL reference space, as described in the following subsection, together with the cc-pVDZ basis set<sup>52</sup> were used. For the saddle point search on the T<sub>1</sub> surface of acetylene, state-averaged CASSCF(6,6) calculations, including the electronic ground state S<sub>0</sub> and the T<sub>1</sub> state, and MR-CISD calculations with a CAS(4,4) reference configuration set (as described in more detail in the respective subsection below) were carried out.

In Table 1 the number of RGF iteration steps for the two test cases and the three options for the treatment of the Hessian mentioned above are given. Table 1 shows that the number of RGF steps does not vary too much for searches using different options for calculating the Hessian. The number of corrector steps per predictor step ranges between two and three on the average. The calculations for case 2 work very well in all cases and are, of course, the preferred ones. It is interesting to note that in the searches SP  $\rightarrow$  *cis*-acetylene updating the Hessian leads to a smaller number of iterations than for case 1 where the Hessian is calculated exactly. Case 3 is more time consuming and should be reserved for difficult situations where the Hessian update does not work.

#### The $H_2CO$ PES

In the first step of the search for stationary points on the  $S_0$  PES of  $H_2CO$ , the RGF method and the closed shell SCF calculations were used. After a successful localization of stationary points, final GDIIS geometry optimizations were performed using the MR-CISD and MR-AQCC methods and the cc-pVTZ basis set.<sup>52</sup> For the construction of the reference configurations a reduced valence CAS (REDVAL) space was defined. The active space consisted of the valence orbitals (1b<sub>2</sub>, 5a<sub>1</sub>, 1b<sub>1</sub>, 2b<sub>2</sub>, 2b<sub>1</sub>, 6a<sub>1</sub>, 3b<sub>2</sub>,



Figure 1. Stationary points on the  $H_2CO$  PES. Relative energies (kcal/mol) were computed with the REDVAL-2ex-AQCC method and the cc-pVTZ basis set.

and 7a<sub>1</sub>) and eight valence electrons. The  $1a_1 - 4a_1$  orbitals were kept doubly occupied. The REDVAL space was used in all MCSCF calculations. The reference space for the MR-CISD and MR-AQCC calculations was reduced for computational economy from REDVAL to REDVAL-2ex, which consisted of all one- and two-electron excitations from the four strongly occupied MCSCF orbitals (1b<sub>2</sub>, 5a<sub>1</sub>, 1b<sub>1</sub>, and 2b<sub>2</sub>) into the remaining four orbitals (2b<sub>1</sub>, 3b<sub>2</sub>, 6a<sub>1</sub>, and 7a<sub>1</sub>) of the REDVAL space. The final expansion space consisted of the reference configurations and all single and double excitations from the reference configurations into all active and virtual orbitals. The 1a<sub>1</sub> and 2a<sub>1</sub> core orbitals were frozen in all post-MCSCF calculations.

Based on the extensive searches for stationary points reported in refs. 18 and 31 the most stable minimum structures and connecting saddle points were chosen. An overview of the selected structures and of the notation used can be found in Figure 1. Four minima, consisting of the  $C_{2v}$  global minimum structure  $M_1$  of formaldehyde, the dissociation product  $H_2$ +CO ( $M_2$ ), and the *trans*- ( $M_3$ ) and *cis*-hydroxycarbene ( $M_4$ ), were investigated. Starting from these minima, five first-order saddle points ( $F_1$ - $F_5$ ) and one second-order saddle point,  $S_1$ , connecting the different minimum structures as indicated in the figure, were determined.

Geometries for structures  $M_1$  and  $F_4$  and relative stabilities are collected in Table 2. Table 3 shows results for the dissociation products CO and  $H_2$  (structure  $M_2$ ), and results calculated for  $M_3$ ,

 $M_4$ ,  $F_1$ ,  $F_2$ ,  $F_3$ , and  $F_5$  are given in Table 4. For all structures zero-point energy corrections were determined as well using respective single-reference calculations. In the case of the  $M_1$  structure the REDVAL-2ex reference space was tested against the full REDVAL space. As Table 2 shows, REDVAL-2ex geometries—computed at a significantly reduced computational cost—are in very good agreement with the full REDVAL results. Therefore, the former reference space was used in the following calculations on the remaining formaldehyde structures instead of the full RED-VAL approach. For comparison, experimental geometries and CCSD(T) results reported by Feller et al.<sup>30</sup> using an aug-cc-pVTZ basis set are given for the  $M_1$  structure as well. All MR methods used in the present work show very good agreement with each other and with the CCSD(T) results. Agreement with experimental geometry data is also good.

The saddle point  $F_4$  leading to the dissociation products CO and  $H_2$  was investigated extensively in previous investigations by several authors.<sup>18,26–32</sup> The REDVAL-2ex results agree quite well with the CCSD/CCSDT-1 results of Scuseria and Schaefer<sup>26</sup> (TZ+2P; see Table 2) and those reported by Feller et al.<sup>30</sup> (basisset extrapolated barrier height 87.4 kcal/mol). Results for the dissociation products CO and  $H_2$  and the reaction energy for the dissociation  $H_2CO \rightarrow H_2+CO$  are collected in Table 3. Reaction energies  $\Delta E_e$  (REDVAL-2ex-AQCC) are too small by 0.7 kcal/

Method <sup>a</sup>	Case 1 <sup>b</sup>	Case 2 <sup>b</sup>	Case 3 <sup>b</sup>
Hydroxycarbene <sup>c</sup>			
SCF (SCF)			
$M_3 \rightarrow F_1$	14 (6)	16 (6)	15 (6)
$F_1 \rightarrow M_4$	18 (6)	18 (6)	20 (6)
SR-CISD (SCF)			
$M_3 \rightarrow F_1$	17 (6)	19 (6)	17 (6)
$F_1 \rightarrow M_4$	20 (6)	23 (6)	19 (6)
Acetylene $(T_1)^d$			
MCSCF (MCSCF)			
$trans \rightarrow SP^{e}$	12 (6)	13 (6)	11 (6)
$SP^e \rightarrow cis$	25 (7)	18 (6)	17 (6)
MR-CISD (MCSCF)			
$trans \rightarrow SP^{e}$	13 (6)	12 (6)	11 (6)
$SP^e \rightarrow cis$	30 (8)	23 (7)	21 (7)

 Table 1. Total Number of RGF Steps for Various Approximations Used for the Hessian Matrix Calculations.

**Table 3.** Optimized Bond Lengths (Å) for CO and  $H_2$  and the Reaction Energy for  $H_2CO \rightarrow H_2 + CO$  (kcal/mol).

Method	$R_{\rm CO}$	$R_{\rm HH}$	$\Delta E_e{}^{\rm a}$	$\Delta E_0{}^{\mathrm{a,b}}$
REDVAL-2ex-CISD	1.134	0.738	2.9 (4.6)	$-4.9(-3.2)^{c}$
REDVAL-2ex-AQCC	1.135	0.741	4.5	-3.1 <sup>d</sup>
CCSD/CCSDT-1e,26	1.126	0.741	2.7	
Exp.	1.12855	0.741 <sup>55</sup>	5.2 <sup>f</sup>	$-2.2^{56}$

 $^{a}\Delta E_{\text{MR-CISD+Q}}$  in parentheses.

<sup>b</sup>Including ZPE correction.

<sup>c</sup>ZPE correction from SR-CISD.

<sup>d</sup>ZPE correction from SR-AOCC.

eCCSD geometry and CCSDT-1 energy at CCSD geometry.

<sup>f</sup> See ref. 26 for the determination of this value.

<sup>a</sup>Method for Hessian calculation in parentheses.

<sup>b</sup>For the definition of cases see text. Number of predictor steps in parentheses.

<sup>c</sup>Search direction  $\angle$ HCOH; predictor step length = 0.15 rad; corrector step convergence criterion 0.001 aJ/Å and aJ/rad for stretching coordinates and angular coordinates, respectively; cc-pVDZ basis set; for the definition of individual cases see text.

<sup>d</sup>Search direction  $\angle$ HCCH; predictor step length = 0.1 rad; corrector step convergence criterion 0.001 aJ/Å and aJ/rad for stretching coordinates and angular coordinates, respectively; cc-pVDZ basis set; for the definition of individual cases see text.

<sup>e</sup>Out-of-plane saddle point.

mol as compared to the experimental value. In the extrapolated results by Feller et al.,<sup>30</sup> a value of 5.8 kcal/mol was obtained.

For the remaining structures investigated in this work less extensive calculations using either SCF,<sup>18,31</sup> SR-CISD,<sup>23</sup> or

QCISD<sup>31</sup> method with basis sets of, at most, polarized DZ quality have been carried out so far. Thus, in these cases our results are expected to give additional information with significantly improved accuracy. Optimized geometries of the s-trans hydroxycarbene M3 and s-cis hydroxycarbene M4 and relative stabilities are collected in Table 4. Starting from the s-trans hydroxycarbene M<sub>3</sub>, RGF searches were performed with search directions ∠HCOH,  $\angle$ HCO, and  $\angle$ HOC leading to the saddle points F<sub>1</sub>, F<sub>3</sub>, and S<sub>1</sub>, respectively (see also Fig. 1). In Table 4 comparison is also made with SCF/QCISD results obtained by Jensen<sup>31</sup> and the DFT-BP calculations of Deng et al.<sup>27</sup> as typical representations of previous results available in the literature. Comparing the latter results with the REDVAL-2-ex-AQCC of this work, one finds in many cases acceptable agreement. However, some noteworthy deviations are also observed: in the case of  $F_1$ ,  $\approx 6^\circ$  in the HOC angle and  $\approx 0.04$ Å in  $R_{CH}$  for  $F_2$  using the DFT-BP method. For  $\Delta E_e$  values we observed in the case of QCISD results deviations of ≈4 kcal/mol for F<sub>2</sub>,  $\approx$ 9 kcal/mol for F<sub>3</sub>, and  $\approx$ 7 kcal/mol for F<sub>5</sub>. Different

**Table 2.** Optimized Bond Lengths (Å), Angles (deg), and Energies Relative to Structure  $M_1$  (kcal/mol) for Structures  $M_1$  and  $F_4$  of H<sub>2</sub>CO.

	$R_{\rm CO}$	R <sub>CH1</sub>	$R_{\rm CH2}$	$\angle H_1 CO$	$\angle H_2CO$	$\Delta E_e{}^{\rm a}$	$\Delta E_0^{a,b}$
M <sub>1</sub>							
REDVAL-2ex-CISD	1.208	1.100	1.100	121.9	121.9	_	_
REDVAL-CISD	1.209	1.101	1.101	121.9	121.9	_	_
REDVAL-2ex-AQCC	1.209	1.103	1.103	121.9	121.9	_	_
REDVAL-AQCC	1.210	1.104	1.104	121.9	121.9	_	_
CCSD(T) <sup>30</sup>	1.211	1.103	1.103	121.8	121.9	_	_
Exp. <sup>54</sup>	1.203	1.100	1.100	121.8	121.8	_	_
F <sub>4</sub>							
REDVAL-2ex-CISD	1.170	1.089	1.679	163.7	111.5	86.8 (86.9)	81.4 (81.5) <sup>c</sup>
REDVAL-2ex-AQCC	1.171	1.093	1.675	163.6	111.5	87.1	81.8 <sup>d</sup>
CCSD/CCSDT-1 <sup>e,26</sup>	1.163	1.093	1.661	163.1	111.3	86.8	81.4

 ${}^{a}\Delta E_{MR-CISD+Q}$  in parentheses.

<sup>b</sup>Including ZPE corrections.

<sup>c</sup>ZPE correction from SR-CISD.

<sup>d</sup>ZPE correction from SR-AQCC.

eCCSD geometry and CCSDT-1 energy at CCSD geometry.

Table 4.	Optimized	Bond	Lengths	(A), .	Angles	(deg),	and	Energies	Relative	to	Ground	State M <sub>1</sub>	(kcal/mol)
for the S	Structures N	13, M4	, F <sub>1</sub> , F <sub>2</sub> ,	F <sub>3</sub> , ai	nd F <sub>5</sub> o	f H <sub>2</sub> CO	D.						

	$R_{\rm CO}$	$R_{\rm CH}$	R <sub>OH</sub>	∠HCO	∠HOC	∠HOCH	$\Delta E_e{}^{\mathrm{a}}$	$\Delta E_0^{a,b}$
M <sub>3</sub>								
REDVAL-2ex-CISD	1.317	1.107	0.966	102.2	107.1	180.0	53.0 (52.4)	53.1 (52.5) <sup>c</sup>
REDVAL-2ex-AQCC	1.319	1.113	0.966	102.0	107.2	180.0	52.4	52.5 <sup>d</sup>
SCF/QCISD <sup>e,31</sup>	1.299	1.102	0.974				54.0	
DFT-BP <sup>27</sup>	1.320	1.125	0.978	102.3	108.1	180.0	52.5	52.5
M <sub>4</sub>								
REDVAL-2ex-CISD	1.314	1.121	0.970	106.5	113.6	0.0	57.5 (56.8)	57.1 (56.5) <sup>c</sup>
REDVAL-2ex-AQCC	1.316	1.122	0.971	106.5	113.9	0.0	58.0	57.4 <sup>d</sup>
SCF/QCISD <sup>e,31</sup>	1.297	1.110	0.949				59.0	
DFT-BP <sup>27</sup>	1.314	1.131	0.987	108.2	116.2	0.0	56.8	56.2
F <sub>1</sub>								
REDVAL-2ex-CISD	1.360	1.119	0.961	104.8	114.2	90.4	82.8 (82.6)	80.1 (80.0) <sup>c</sup>
REDVAL-2ex-AQCC	1.360	1.125	0.964	104.8	114.9	91.7	82.2	79.6 <sup>d</sup>
SCF/QCISD <sup>e,31</sup>	1.344	1.113	0.946				85.0	
DFT-BP <sup>27</sup>	1.353	1.142	0.969	104.9	121.3	90.1	82.5	80.3
F <sub>2</sub>								
REDVAL-2ex-CISD	1.309	1.103	1.174	114.5	60.1	180.0	87.2 (86.4)	83.2 (82.4) <sup>c</sup>
REDVAL-2ex-AQCC	1.311	1.087	1.177	114.5	60.0	180.0	86.6	82.2 <sup>d</sup>
SCF/QCISD <sup>e,31</sup>	1.270	1.097	1.171		59.3	180.0	91.0	
DFT-BP <sup>27</sup>	1.316	1.124	1.176	114.4	61.5	180.0	81.7	78.1
F <sub>3</sub>								
-							120.7	119.0
REDVAL-2ex-CISD	1.286	1.056	0.981	178.7	111.5	180.0	(119.6)	(118.0) <sup>c</sup>
REDVAL-2ex-AQCC	1.289	1.060	0.982	178.4	111.5	180.0	118.4	116.6 <sup>d</sup>
SCF/QCISD <sup>e,31</sup>	1.279	1.049	0.954				127.0	
F <sub>5</sub>								
							109.8	103.8
REDVAL-2ex-CISD	1.280	1.355	1.221	101.0	65.7	0.0	(107.6)	(101.7) <sup>c</sup>
REDVAL-2ex-AQCC	1.281	1.365	1.223	101.1	65.7	0.0	107.7	101.8 <sup>d</sup>
SCF/QCISD <sup>e,31</sup>	1.235	1.430	1.174	97.9	70.0	0.0	115.0	
DFT-BP <sup>27</sup>	1.288	1.373	1.232	102.5	65.7	0.0	103.6	98.1

 $^{a}\Delta E_{MR-CISD+Q}$  in parentheses.

<sup>b</sup>Including ZPE correction.

<sup>c</sup>ZPE correction from SR-CISD.

<sup>d</sup>ZPE correction from SR-AQCC.

eSCF geometry and QCISD energy at SCF geometry [basis set 6-31G(d,p)].

characterizations of structure  $S_1$  (see Fig. 1) have been given in previous studies. It has been reported to be a first-order saddle point in DFT calculations<sup>28</sup> and to be a second-order saddle point by Jensen.<sup>31</sup> The present investigations (SR-CISD/cc-pVDZ) showed that this structure is a second-order saddle point. Therefore, we did not perform further investigations on it as we were interested only in first-order saddle points. The saddle point  $F_2$ (symmetry  $C_s$ ), located between structure  $M_1$  and the *s*-trans hydroxycarbene  $M_3$ , is of first-order and not of second-order as found in the STO-3G/SCF investigations by Quapp et al.<sup>18</sup>

# Acetylene

The planar and nonplanar saddle points on the PES of acetylene in the first two triplet states ( $T_1$  and  $T_2$ ) and the linear ground state geometry were investigated. The RGF saddle point search was performed at the MCSCF level in the cc-pVDZ basis;<sup>52</sup> for the

subsequent GDIIS geometry refinement MR-CISD and MR-AQCC calculations and the cc-pVTZ basis<sup>52</sup> set were used. Only the MR-AQCC results, which are considered to be the more accurate ones, are presented here. The active space in the MCSCF calculations consisted of a CAS of six electrons in six orbitals  $(3\sigma_{\rm g}, 1\pi_{\rm u}, 1\pi_{\rm g}, \text{ and } 3\sigma_{\rm u} \text{ in } D_{\infty \rm h} \text{ notation})$ . Because the present calculations are part of a more extensive survey on several excitedstate acetylene surfaces, state-averaged MCSCF calculations, including the ground state, the three lowest triplet states, and the two lowest singlet states, were performed in order to get a balanced description of these states. The MR-CISD reference space was constructed from a CAS of four electrons in four orbitals  $(1\pi_u,$  $1\pi_{o}$ ). The expansion space consisted of the reference configurations and all single and double excitations into all active and virtual orbitals. The 1s orbitals of carbon were kept frozen in all post-MCSCF calculations.

**Table 5.** Optimized Bond Lengths (Å), Angles (deg), and Relative Energies (eV) for Minima and Saddle Points on the  $S_0$ ,  $T_1$ , and  $T_2$  Surfaces of Acetylene Calculated at the MR-AQCC Level Using the cc-pVTZ Basis Set.

	Rec	Rem	Reup	/ H.CC	/H <sub>2</sub> CC	/ H.CCH	$\Delta E^{a}$	Ref
		A CHI	ACH2	211/00		211/00112	<b>_</b> e	
$1^{1}\Sigma_{a}^{+}$ (Ground state, $D_{ob}$ )								
MR-AQCC	1.210	1.061	1.061	180.0	180.0	_		This work
$1^{3}B_{2}$ ( <i>cis</i> min., $C_{2y}$ )								
MR-AQCC	1.341	1.087	1.087	128.5	128.5	0.0	3.84	This work
CCSD(T)	1.340	1.091	1.091	128.0	128.0	0.0	3.83	Ref. 39
$1^{3}B_{\mu}$ (trans min., $C_{2h}$ )								
MR-AQCC	1.349	1.079	1.079	132.2	132.2	180.0	4.14	This work
CCSD(T)	1.345	1.082	1.082	131.5	131.5	180.0	4.18	Ref. 39
$1^{3}A'$ (Planar saddle pt., C <sub>s</sub> )								
MR-AQCC	1.344	1.085	1.060	128.8	175.6	180.0	0.55	This work
SR-CISD/CCSD(T) <sup>b</sup>	1.325	1.088	1.059	127.3	174.0	180.0	0.62	Ref. 36
$1^{3}B$ (oop saddle point, $C_{2}$ )								
MR-AQCC	1.366	1.077	1.077	139.6	139.6	106.5	0.58	This work
$1^{3}A_{2}$ (cis min., $C_{2v}$ )								
MR-AQCC	1.359	1.091	1.091	130.4	130.4	0.0	4.81	This work
CCSD(T)	1.360	1.095	1.095	130.3	130.3	0.0	4.79	Ref. 39
$1^{3}A_{u}$ (trans min., $C_{2h}$ )								
MR-AQCC	1.385	1.091	1.091	120.7	120.7	180.0	4.49	This work
CCSD(T)	1.386	1.094	1.094	120.5	120.5	180.0	4.47	Ref. 39
$1^{3}A''$ (Planar saddle pt., C <sub>s</sub> )								
MR-AQCC	1.365	1.104	1.067	119.9	179.8	180.0	0.30	This work
EOM-CCSD	1.360	1.100	1.065	118.2	179.9	180.0	0.26	Ref. 38
$1^{3}$ A (oop saddle point, C <sub>2</sub> )								
MR-AQCC	1.352	1.079	1.079	143.0	143.0	91.7	0.66	This work

<sup>a</sup>Minimum-to-minimum excitation energies for minimum structures and energy barriers relative to the *cis* geometry for saddle points.

<sup>b</sup>Optimized SR-CISD geometry and TZ CCSD(T) energies.

The linear ground state geometry and the *cis*- and *trans*-minima on the T<sub>1</sub> and T<sub>2</sub> surfaces were optimized first. Both the *cis*- and *trans*-minima are strongly bent, and  $R_{\rm CC}$  is stretched by about 0.15 Å as compared to the ground state (see Table V). For comparison, optimized geometries obtained by Sherill et al.<sup>39</sup> from cc-pVTZ CCSD(T) calculations are given in Table V as well. They agree very well with our results. Preliminary basis set extrapolations<sup>43</sup> based on MR-AQCC calculations gave for the cis T<sub>1</sub> (1<sup>3</sup>B<sub>2</sub>) structure an excitation energy of 3.93 eV, in very good agreement with the extrapolated value of 3.91 reported by Sherill et al.<sup>39</sup> Zero-point corrections reduce this excitation energy by  $\approx 0.05$  eV. Thus, we agree with the conclusion of the just-mentioned authors that the experimental estimate of 3.58 eV (28,900 cm<sup>-1</sup>)<sup>53</sup> for  $\Delta E_0$ is too low.

Using the RGF method two types of saddle points were determined for the  $T_1$  and  $T_2$  states: a planar one of  $C_s$  symmetry and a nonplanar one of  $C_2$  symmetry. The planar saddle point for the  $T_1$  state is of second order. All other saddle points are of first order. The planar saddle point structure can be compared to the SR-CISD results of Vacek et al.,<sup>36</sup> which show typical deviations of SR-CISD towards smaller bond distances as compared to the present MR results. SR calculations on the  $T_2$  state meet problems because instabilities for the SCF wave functions have been found by Yamaguchi et al.<sup>35</sup> Therefore, the possibility of performing MR calculations based on MCSCF wave functions is of particular importance here and in general for higher excited states. For the planar saddle point in the T<sub>2</sub> state, comparison can be made with the EOM-CCSD calculations performed by Sherrill et al.<sup>38</sup> Agreement with our results is quite good. To our knowledge, out-ofplane saddle points have been investigated only by Cui et al.<sup>40,41</sup> based on CASSCF and EOM-CCSD calculations. In these cases the reference wave function is dominated by a 1:1 mixture of two configurations and a multireference approach is mandatory. In this work the first post-CASSCF results are presented. In both cases (1<sup>3</sup>A and 1<sup>3</sup>B) substantial barriers of  $\approx 0.6$  eV with respect to the planar cis structure are observed. In particular, the out-of-plane saddle point of the 1<sup>3</sup>A state is of interest. This state crosses for nonplanar geometries with the next higher triplet state, 2<sup>3</sup>B. As has been shown by Cui et al.,41 this crossing is important for the understanding of the photodissociation of acetylene.

## Conclusions

The implementation of the RGF procedure into the COLUMBUS program system resulted in a very useful tool for the search and optimization of stationary points at the multireference level for ground states as well as excited states. Because of the generality of the multireference approach very general and difficult situations can be treated, which leads to new possibilities for accurate determinations of stationary points.

RGF searches were performed for the  $H_2CO$  system on the  $S_0$  PES and for acetylene on the  $T_1$  and  $T_2$  PES. In total, eight stationary points for  $H_2CO$  and nine stationary points for acetylene have been investigated using the MR-CISD and MR-AQCC methods, respectively. In the case of the transition structures involving hydroxycarbene, the present MR-CISD/AQCC results are a significant improvement compared to previous calculations. In the case of the planar structure  $F_2$  (see Fig. 1), we confirm previous findings<sup>23</sup> that it is a first-order saddle point and not of second order as found in the STO-3G/SCF investigations by Quapp et al.<sup>18</sup> This is another example of the observation<sup>31</sup> that the number of imaginary frequencies characterizing a saddle point can depend strongly on the computational level. Starting from the *cis*- and *trans*-minima on the  $T_1$  and  $T_2$  surfaces of acetylene, planar and nonplanar saddle points were located.

# Acknowledgments

The authors acknowledge support from the Austrian Science fund within the framework of the Special Research Program F16 and project P14442-CHE, and from the COST Chemisty/D9, project No. D9/0006/98. We thank one referee for drawing our attention to the advantages of the Hessian update method developed by Bofill.

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